



MEMS AC Current Sensor for use in DR

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Acknowledgement

**Much of the work reported here was
done by Ph.D. student
Eli Leland, working with Dick White
(EECS) and Paul Wright (ME)**





Agenda

- ★ **Size domains for electric sensors**
- ★ **MEMS (Micro-Electro-Mechanical Systems)**
- ★ **Passive, proximity-based electric sensors**
- ★ **Current sensing at potentials < 600 volts**
- ★ **Existing technologies**
- ★ **Permanent magnets and piezoelectric materials**





Size domains for electricity sensors

- ★ **Meter (m, little over a yard)**
- ★ **Millimeter (mm, 10^{-3} meters)**
 - ◆ Grain of sand = 0.2 to 2 mm diameter
- ★ **Micrometer (μm , 10^{-3} mm)**
 - ◆ Human hair ~ 70-100 μm
 - ◆ Domain of electronics and MEMS
- ★ **Nanometer (nm, 10^{-3} μm)**
 - ◆ Molecular bonds are tenths of nm
 - ◆ 1 Angstrom = 0.1 nm

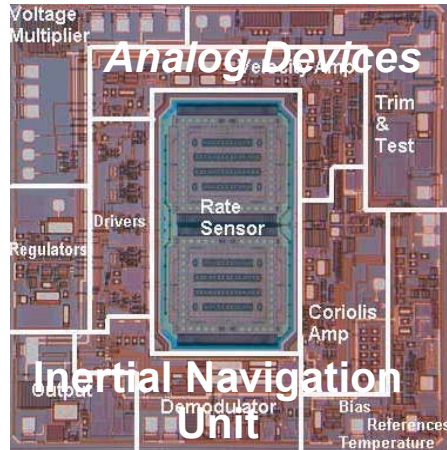
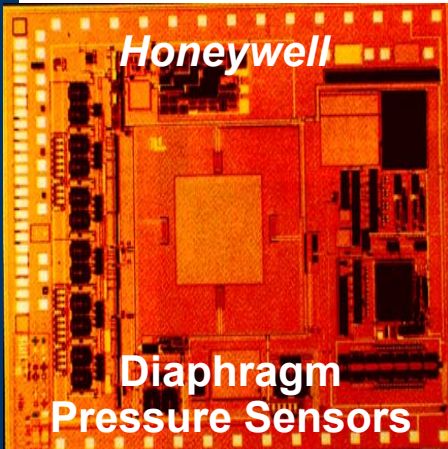




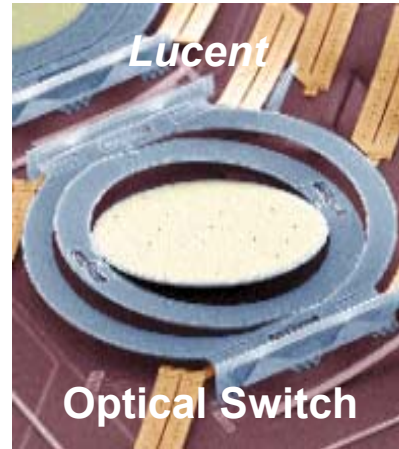
MEMS Examples (Dennis Polla -- DARPA)



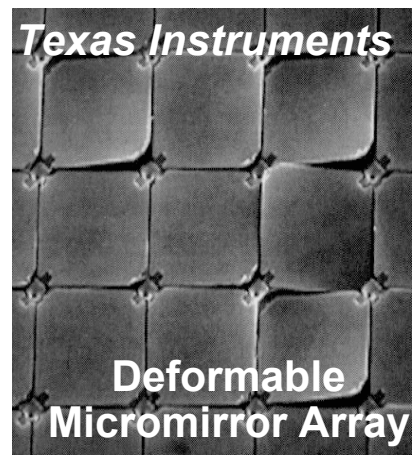
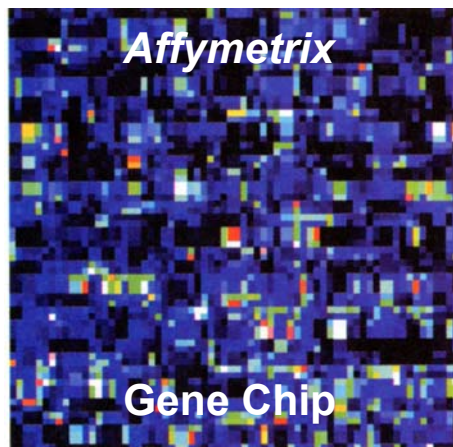
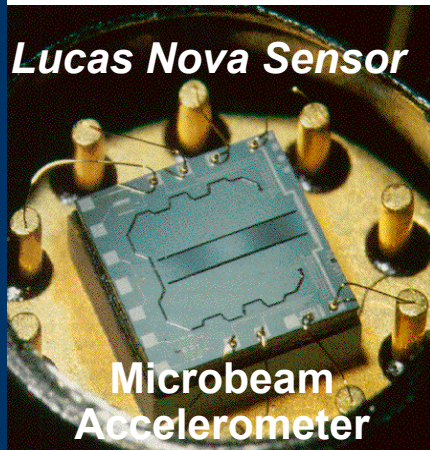
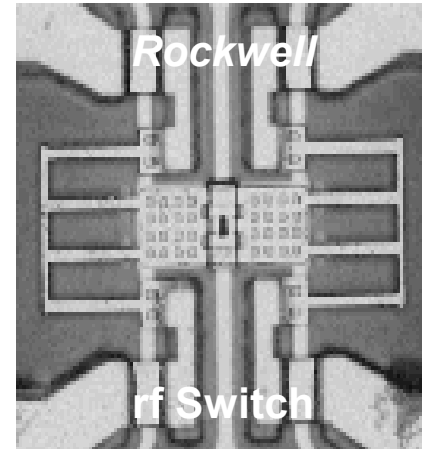
Microsensors



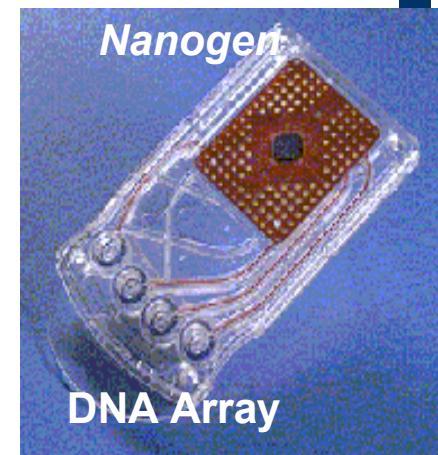
Microactuators



RF Electronics



Microfluidics





Current sensing at potentials <600 v

- * Design **passive, proximity-based** current sensors for homes and buildings
 - ◆ Passive sensors require no external power, dramatically extend life of wireless sensor node
 - ◆ Proximity-based doesn't require electrical connection or wraparound, doesn't require precise alignment to conductor, potentially sensors will be integrated with CPU and radio on a single piece of silicon
- * Focus on currents in and around homes and other buildings (potentials less than 600 volts)

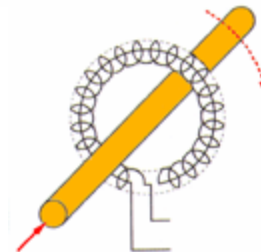




Existing technologies



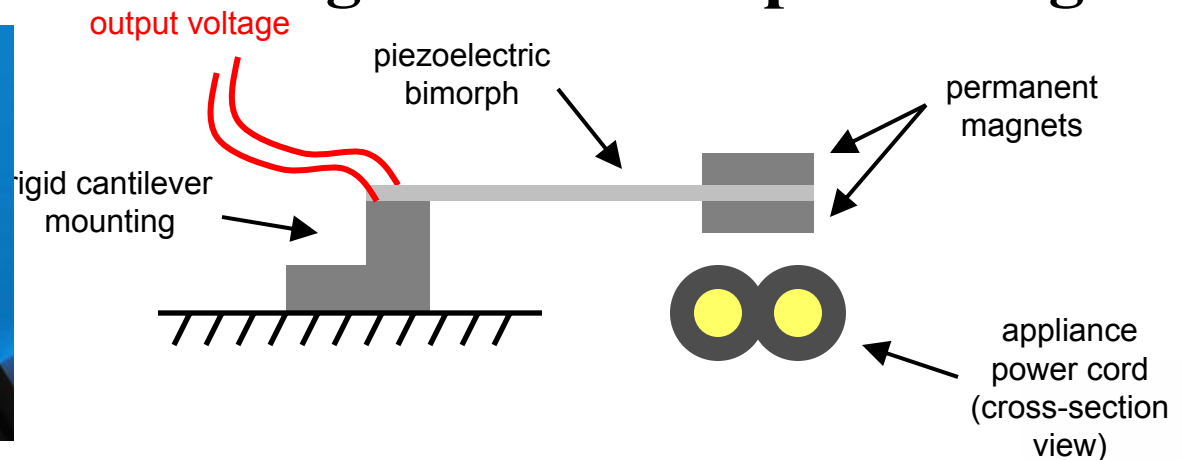
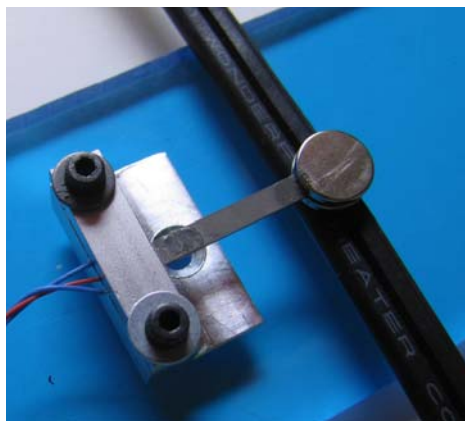
- * **No MEMS current sensor on the market**
- * **No passive (self-powered) sensor on the market that doesn't require wraparound**
- * **Kill-A-Watt™**
 - ◆ shunt resistor-based
 - ◆ in-line
- * **Current Transformer**
 - ◆ self-powered
 - ◆ requires wraparound – impractical for many applications
- * **Hall Sensor**
 - ◆ proximity-based
 - ◆ requires 10s of mW of power
- * **Rogowski Coil**
 - ◆ voltage scales with square of linear dimension so small scales = small voltages
 - ◆ difficult to micro-fabricate a coil of many turns





Basic Idea: Combine permanent magnet and piezoelectric materials in sensor

- ★ Permanent magnets can couple to the magnetic fields surrounding AC current carriers
- ★ Piezoelectric materials can transduce the forces on the permanent magnet to an output voltage

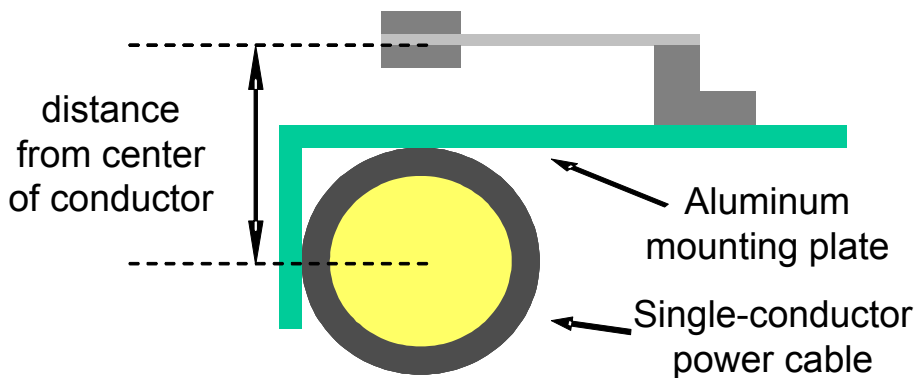
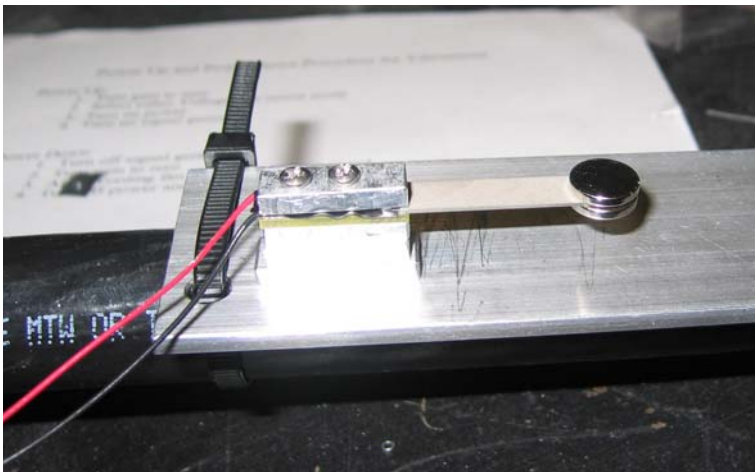




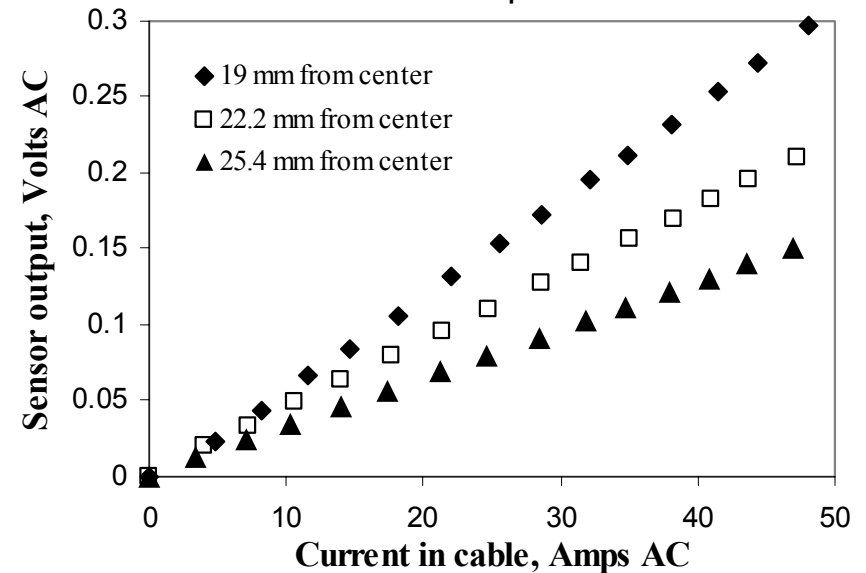
Initial mesoscale prototypes show promising behavior



Sensor mounted on a single-conductor power cable



Current sensor response – varying distance from power cable

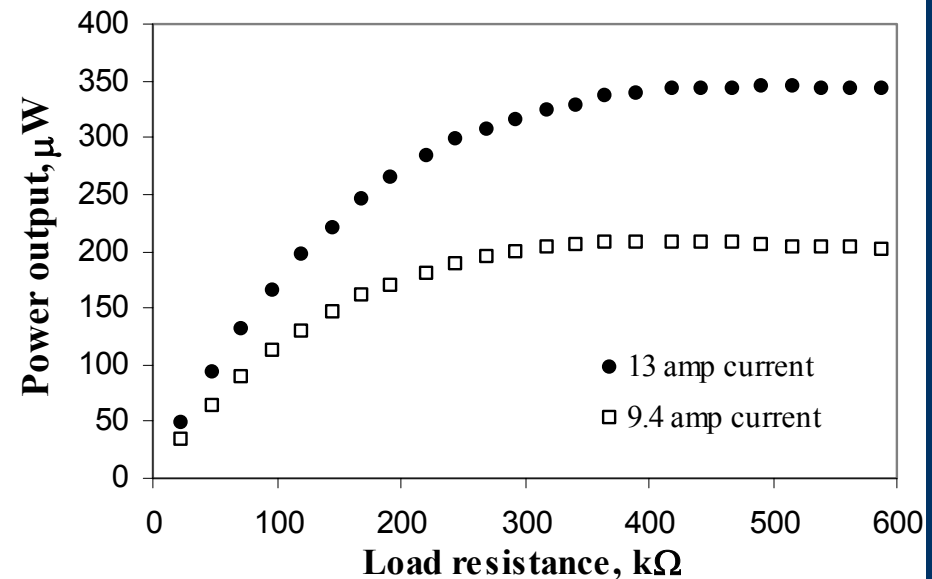




Can we power the sensor node without a battery?

- Device scavenged 350 microwatts from a standard 1500 W space heater appliance cord, sufficient to power a commercially-available wireless sensor node at a 1% duty cycle
- Tuned to 60 Hz resonance frequency for maximum coupling and power output

Energy-scavenging power output by sensor from space heater power cord



Publication:

E. S. Leland, R. M. White, P. K. Wright "Energy scavenging power sources for household electrical monitoring," PowerMEMS 2006, November 29–December 1, 2006, Berkeley, California






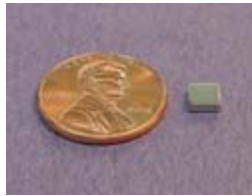
Current sensor design questions

- ★ **How sensitive will the current sensor be?
(in V/A)**
 - ◆ How do I calculate the forces on a permanent magnet in a magnetic field?
 - ◆ How does force on the magnet translate to voltage out of the piezoelectric bimorph transducer?
- ★ **How well will this sensor's performance scale downward to smaller sizes?**

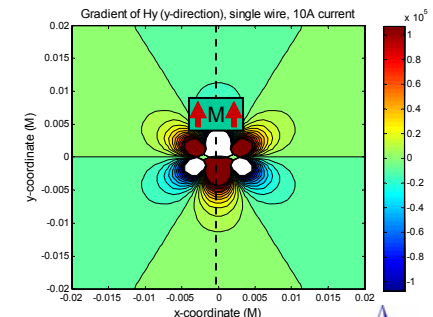
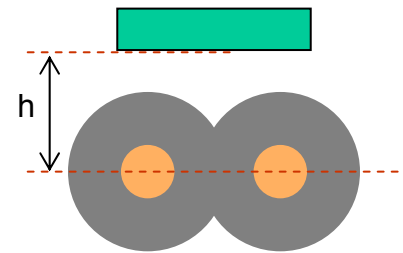


So how big are these forces?

You can feel them!

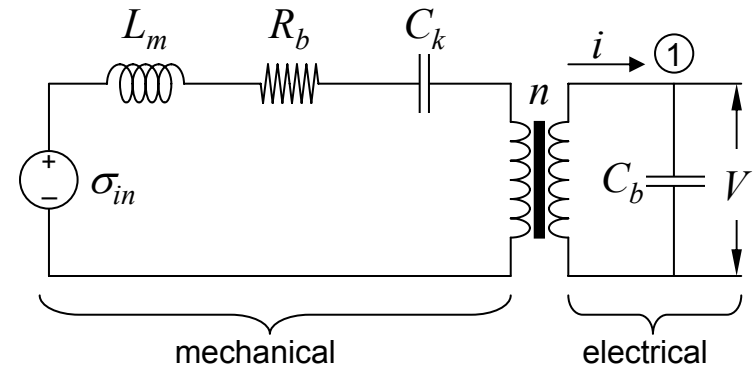
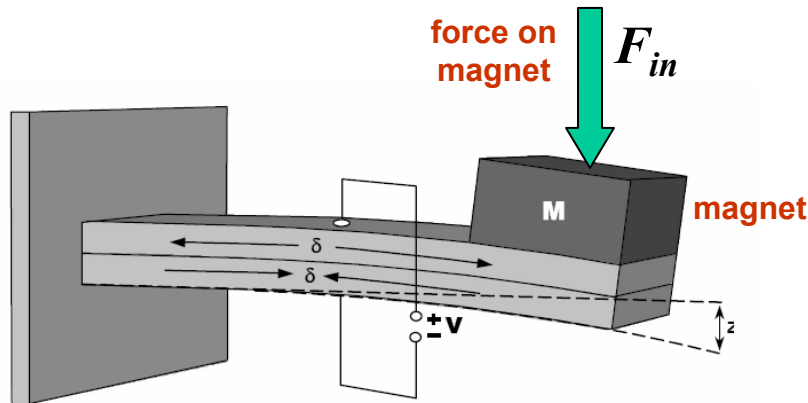
NdFeB magnets (from K & J magnetics www.kjmagnetics.com)		
Dimensions (mm)	3.2 x 3.2 x 1.6	4.8 x 4.8 x 1.6
Mass (g)	0.12	0.27
Br (T)	1.3	1.35
MATLAB simulation results		
Force/Current (mN/A) h = 2 mm	0.446 = 3.8 x gravity at 10 A	0.792 = 3 x gravity at 10 A
Force/Current (mN/A) h = 3 mm	0.254 = 2.2 x gravity at 10 A	0.468 = 1.8 x gravity at 10 A
Force/Current (mN/A) h = 4 mm	0.150 = 1.3 x gravity at 10 A	0.293 = 1.1 x gravity at 10 A

magnet centered above zip-cord





Force on the magnet generates voltage in piezoelectric element



Using electro-mechanical equivalents, applying Kirchhoff's Voltage Law to the left and Kirchhoff's Current Law to the right:

$$\text{KVL: } T_{in} = T_m + T_b + T_k + T_t$$

$$\text{KCL: } i_1 = C_b \dot{V}$$

$$T_{in} = L_m \dot{S} + R_b \dot{S} + \frac{1}{C_k} S + nV$$

To determine equations of motion, we need to find equivalent expressions for T_{in} , L_m , R_b , C_k , n , i , C_b

S. Roundy, P. Wright, "A piezoelectric vibration based generator for wireless electronics," *Smart Materials and Structures*, vol. 13 (2004) pp. 1131-1142





Simulations indicate micro-scale versions should produce measurable voltages



	PZT					Aluminum Nitride	
	prototype bimorph	sputtered film	1 mm PZT MEMS	500 μm MEMS	200 μm MEMS	500 μm MEMS	200 μm MEMS
cantilever l x w (μm)	25 x 3.1 mm	5 x 1 mm	1000 x 100	500 x 100	200 x 50	500 x 100	200 x 50
magnet l x w x t (μm)	3.2 x 3.2 x 1.6 mm	1 x 1 x 1 mm	100 x 100 x 100	100 x 100 x 100	50 x 50 x 50	100 x 100 x 100	50 x 50 x 50
shim thickness (μm)	127	25	1	1	1	1	1
shim material	steel	steel	Pt	Pt	Pt	Pt	Pt
resonance (Hz)	166	560	281	927	7760	1140	9560
sensitivity (mV/A)	74.6	12.5	1.91	0.911	0.0921	10.6	1.08

With sensitivities 10x those of PZT, model results suggest AlN is worth a closer look as an active material.

Notes: Prototype bimorph had two PZT layers, all others have only one active layer. PZT properties: $d_{31} = -141 \text{ pm/V}$, $\epsilon_r = 1800$, density = 7800 kg/m^3 , $c_p = 66 \text{ GPa}$. AlN properties: $d_{31} = -7.5 \text{ pm/V}$, $\epsilon_r = 9$, density = 3200 kg/m^3 , $c_p = 135 \text{ GPa}$. NdFeB properties: density = 7500 kg/m^3 , $B_r = 1.3 \text{ T}$ for the leftmost two beams, 0.5 T for the rest. Steel properties: $c_p = 200 \text{ GPa}$, density = 7800 kg/m^3 . Pt properties: $c_p = 171 \text{ GPa}$, density = 21450 kg/m^3 .

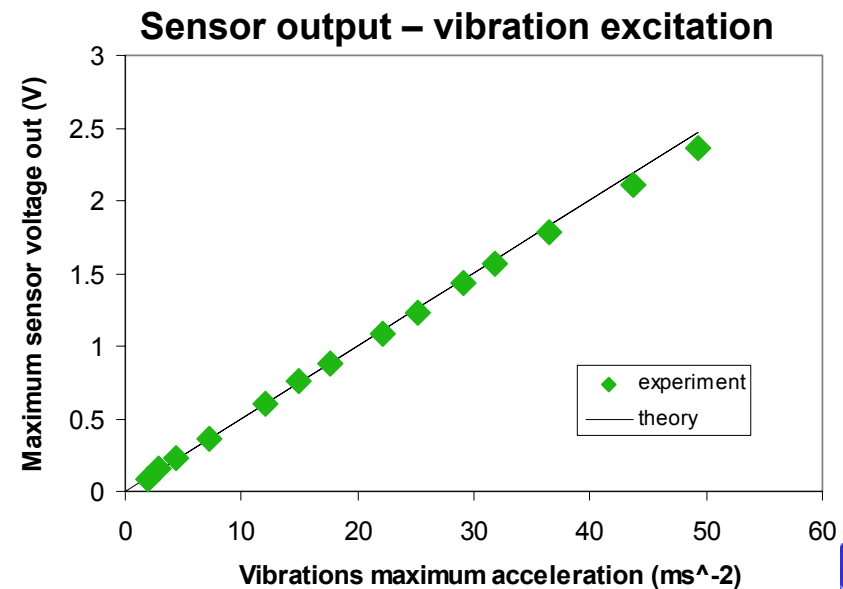
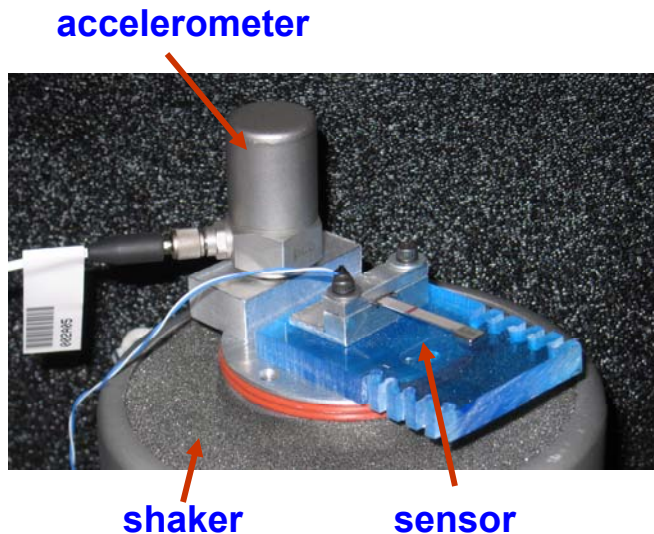




Analysis and experiment in agreement

for mesoscale current sensor

1. Analysis of device output expressed as $V_{out} = F_{in}(d_{31})$ when apply **mechanical force F_{in}** to sensor whose piezo-material is characterized by constant d_{31} . Put sensor device on shake table with known acceleration, measure output and find effective d_{31} by curve fitting





Analysis and experiment in agreement for mesoscale current sensor (continued)



2. Measure **sensor response to current I** , compare with predictions from current sensor analysis using the value of d_{31} obtained from shake table experiment.

Force on cantilever produced by current I is

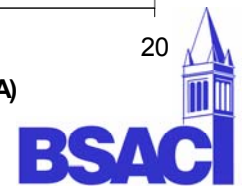
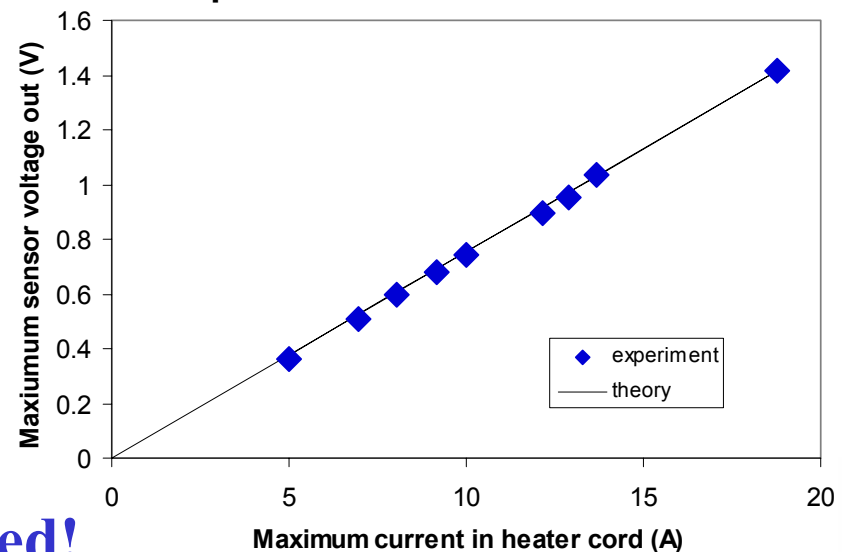
$$F_{in} = I\beta$$



$$V_{out} = I\beta K(d_{31})$$

Excellent agreement observed!

Sensor output – current in heater cord excitation





Major design take-aways

- ★ **Current sensor output voltage is linearly proportional to current, as predicted by theory and demonstrated by experiment**
 - ◆ Magnetic force is proportional to current
 - ◆ Voltage out proportional to force
- ★ **Magnetic force proportional to magnet volume, remanence**
- ★ **Theoretical models suggest micro-scale devices should be feasible**





Research plan going forward

- ★ **Fabricate Aluminum Nitride (AlN) cantilever devices in the UCB Microlab**
- ★ **Characterize AlN cantilevers to verify voltage/force model at the micro-scale**
- ★ **Identify most promising method to fabricate micro-magnets**



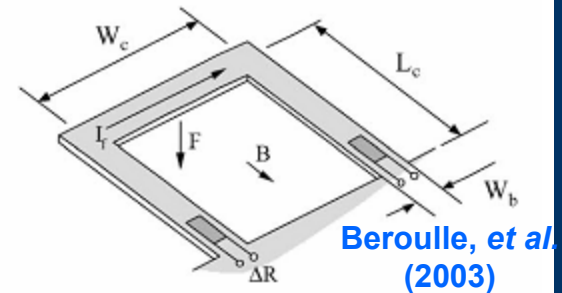


Literature review



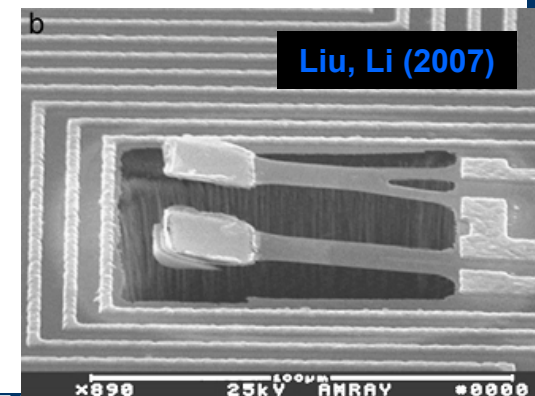
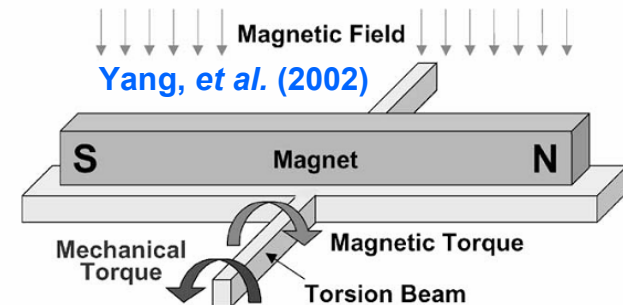
* Measuring current

- C. Xiao, *et al.*, “An Overview of Integratable Current Sensor Technologies,” *Proc. 38th IAS Annual Meeting* (2003) pp. 1251-1258
- P. Ripka, “Current Sensors using Magnetic Materials,” *Journal of Optoelectronics and Advanced Materials*, vol. 6 no. 2 (2004) pp. 587-592



* MEMS magnetometers

- Beroulle, *et al.*, “Monolithic piezoresistive CMOS magnetic field sensors,” *Sensors and Actuators A*, vol. 103 (2003) pp. 23-32
- H.H. Yang, *et al.*, “Ferromagnetic micromechanical magnetometer,” *Sensors and Actuators A*, vol. 97-98 (2002) pp. 88-97
- J. Liu, X. Li, “A piezoresistive microcantilever magnetic field sensor with on-chip self-calibration function integrated,” *Microelectronics Journal*, vol. 38 (2007) pp. 210-215

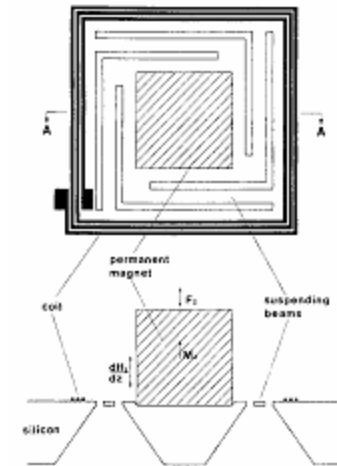
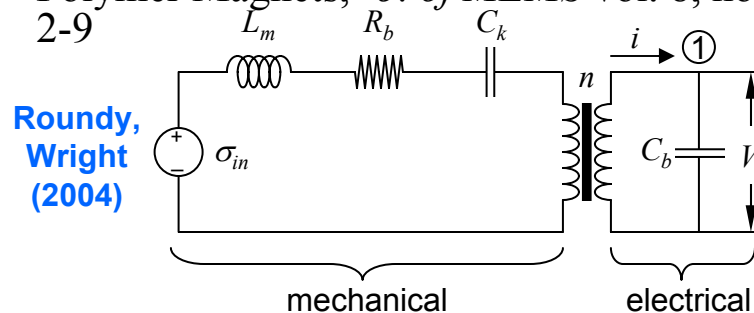


* Piezoelectric cantilever output

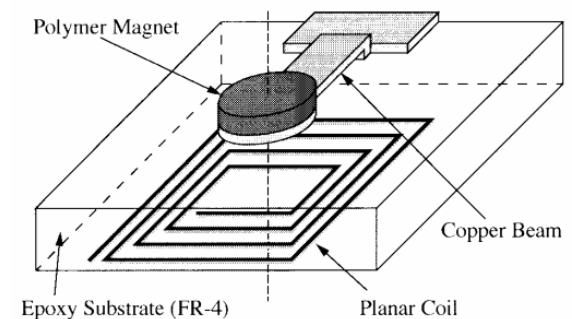
- S. Roundy, P. Wright, "A piezoelectric vibration based generator for wireless electronics," *Smart Materials and Structures* vol. 13 (2004) pp.1131-1142
- S.N. Chen, *et al.*, "Analytical modeling of piezoelectric vibration-induced micro power generator," *Mechatronics* vol. 16 (2006) pp. 379-387

* Magnetic microactuators/sensors

- B. Wagner, W. Benecke, "Microfabricated actuator with moving permanent magnet," *Proc. MEMS '91* (1991) pp. 27-32
- Lagorce, *et al.*, "Magnetic Microactuators based on Polymer Magnets," *J. of MEMS* vol. 8, no. 1 (1999) pp. 2-9



Wagner, Benecke (1991)



Lagorce, et al (1999)



Why not use Hall sensors?

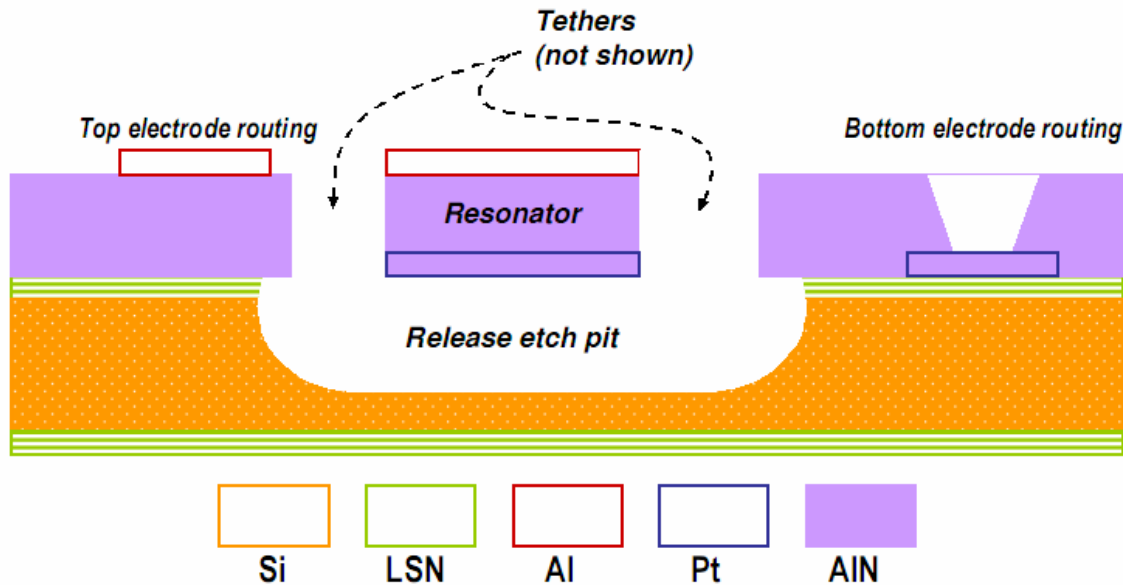
★ Allegro 1392 Hall sensor

- ◆ 9.6 mW average power during operation, 75 μ W sleep
- ◆ Assume duty cycling of 120 samples/sec, 1 millisecond/sample
- ◆ Average power 1.2 mW, ten times the target average power for a sensor node





AlN devices in the UCB Microlab



- ✦ LPCVD low-stress nitride
- ✦ Sputter deposition, pattern, and liftoff of Pt electrode
- ✦ Sputter deposition of AlN film
- ✦ Deposition, patterning, and Cl_2 RIE of Al top electrode
- ✦ Open via to bottom electrode using hot phosphoric acid
- ✦ AlN patterning using LTO “hard mask” and Cl_2 RIE
- ✦ XeF_2 release etch

I'll have to include an elastic support layer, as I'll be fabricating a “31” mode cantilever. SOI substrate is one option.

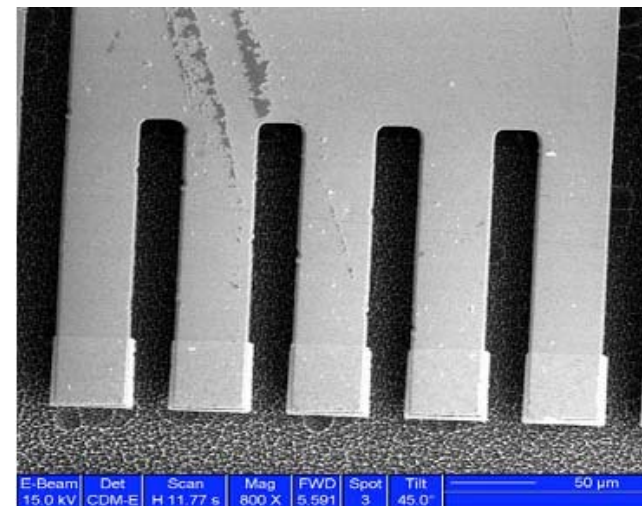
P. Stephanou, “Piezoelectric Aluminum Nitride MEMS Resonators for RF Signal Processing,” *PhD Dissertation*, University of California, Berkeley (2006)





PZT cantilevers in the Microlab pier

1. Single crystal silicon wafer coated with 10 nm SrTiO₃ (STO, from Motorola, Inc.)
2. Deposit SrRuO₃ (SRO) bottom electrode using pulsed laser deposition (PLD)
3. Deposit PZT (PbZr_{0.47}Ti_{0.53}O₃) using PLD
4. Deposit top electrode/elastic layer (Pt with Ti adhesion layer) using e-beam/thermal evaporation
5. Define cantilever structures using photolithography
6. Etch down to Si substrate using ion mill
7. Release cantilever structures using isotropic XeF₂ etch



E. Reilly, E. Carleton, P. Wright, "Thin Film Piezoelectric Energy Scavenging Systems for Long Term Medical Monitoring," *Proc. IEEE Body Sensor Networks 2006* (2006)





Possibilities for magnet fabrication



Screen/direct printing of magnetic powder/polymer composites

- L. Lagorce, M. Allen, "Magnetic and Mechanical Properties of Micromachined Strontium Ferrite/Polyimide Composites," *J. of MEMS* vol. 6 no. 4 (1997) pp. 307-312
- C. Ho, *et al.*, "Dispenser Printed Electrochemical Capacitors for Power Management of Millimeter Scale Lithium Ion Polymer Microbatteries for Wireless Sensors," *Proc. PowerMEMS 2006*, November-December 2006, Berkeley, California, pp. 219-222

Electroplating CoNiMnP, NiFe, Permalloy

- T. Liakopoulos, W. Zhang, C. Ahn, "Electroplated Thick Film CoNiMnP Permanent Magnet Arrays for Micromachined Magnetic Device Applications," *Proc. MEMS '96* (1996) pp. 79-84
- J. Judy, R. Muller, H. Zappe, "Magnetic Microactuation of Polysilicon Flexure Structures," *Journal of MEMS* vol. 4 no. 4 (1995) pp. 162-169

Is NdFeB possible? Is it worth the trouble?

- B. Pawlowski, *et al.*, "NdFeB thick films prepared by tape casting," *J. Magnetism and Mag. Mat'ls* vol. 265 (2003) pp. 337-344
- P. McGuinness, *et al.*, "100- μ m-thick Nd-Fe-B magnets for MEMS applications produced via a low-temperature sintering route," *J. Magnetism and Mag. Mat'ls* vol. 305 (2006) pp. 177-181

