

# Thermoelectric and Piezoelectric Energy Harvesting

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# What to remember:

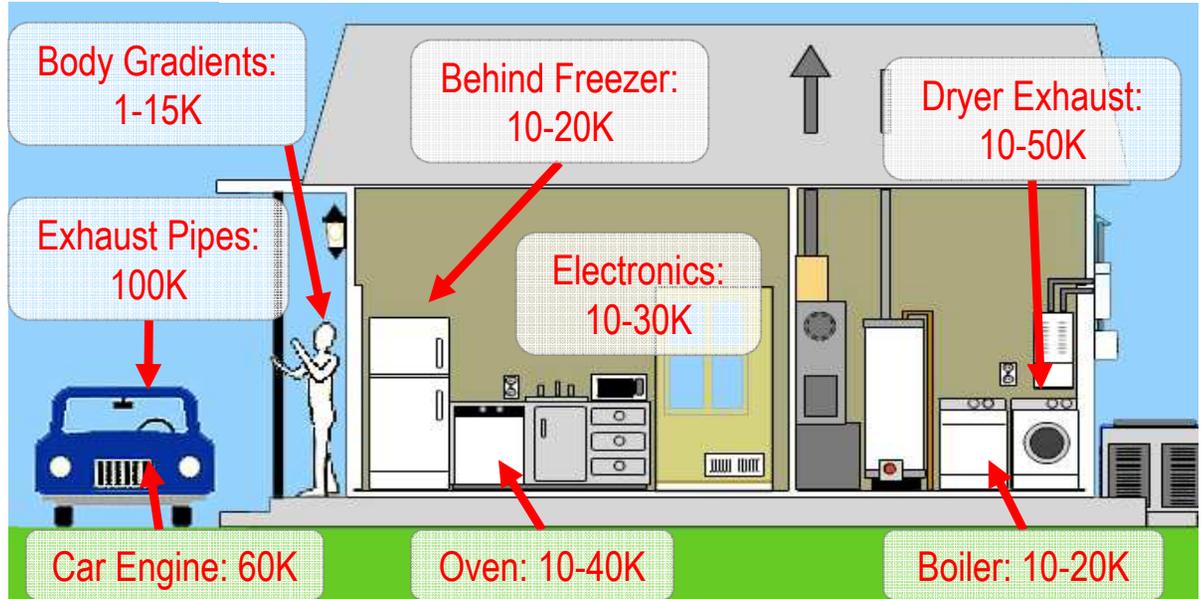
- Thermoelectric
  - Composite materials show promise, further improvements under way
  - Next steps focus on device prototyping
- Piezoelectric
  - Low-frequency resonance attained ( $\sim 31\text{Hz}$ )
  - Voltage output achieved from HVAC duct ( $22\text{ mV}_{\text{rms}}$ )
  - Integration of harvester & capacitor under way

# Energy Harvesting from Waste Heat

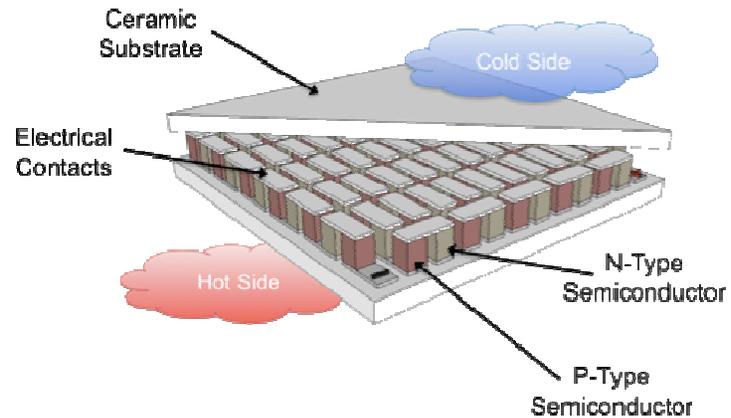
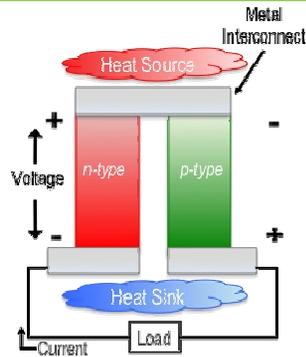
## Alternate applications

Location	Source	Gradient
Factories	Exhaust pipes, Boilers, condensers	10-80K
Vehicles	Engine Exhaust pipes	60K >100K
Airplanes	Cabin to External	10-50K

## Residential temperature gradients

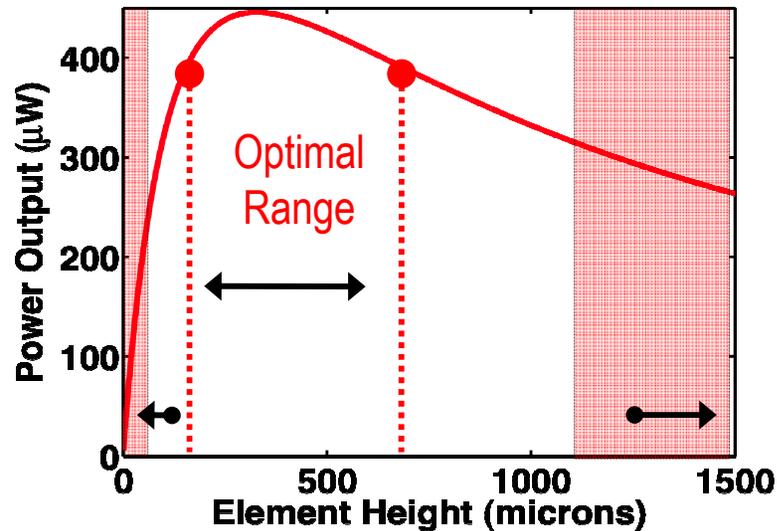


## Thermoelectric Energy Harvesting



# Design of Thermoelectric Devices

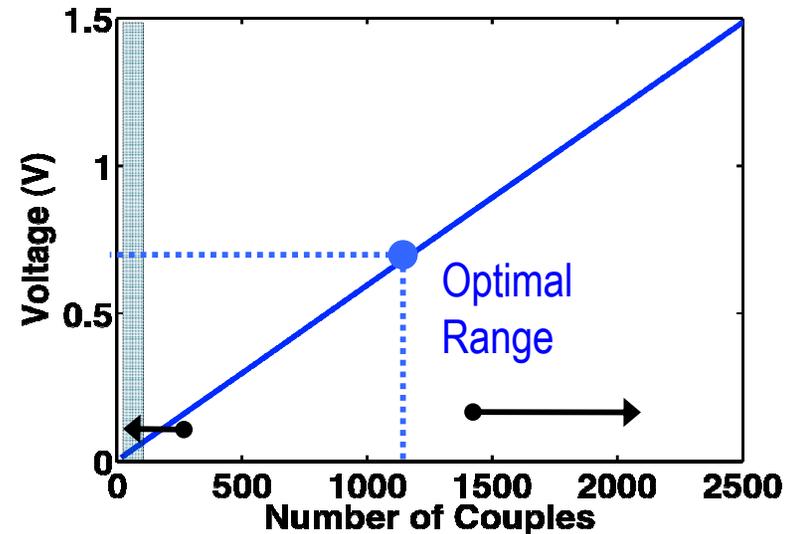
## Power Dependence



Thin film elements

Bulk elements

## Voltage Dependence

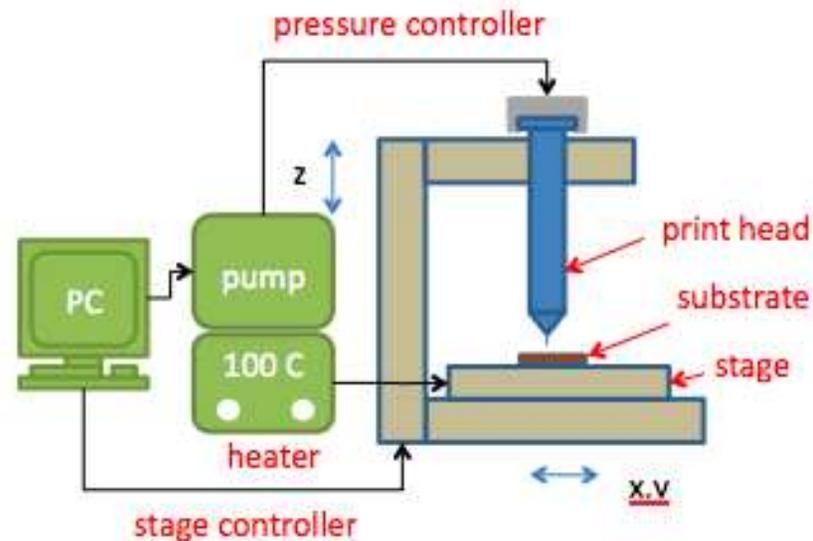
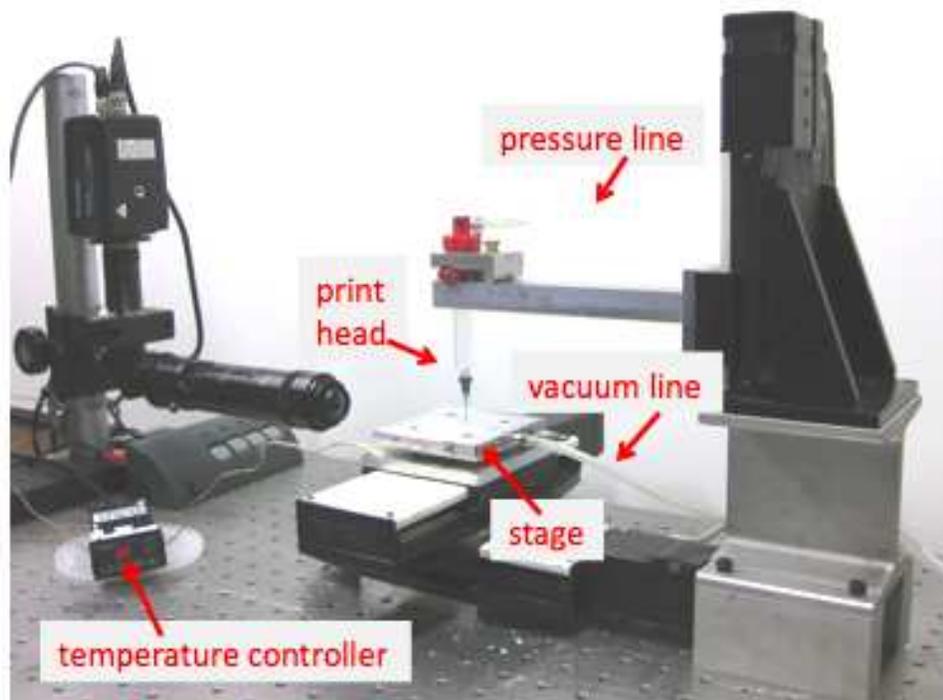


Bulk elements

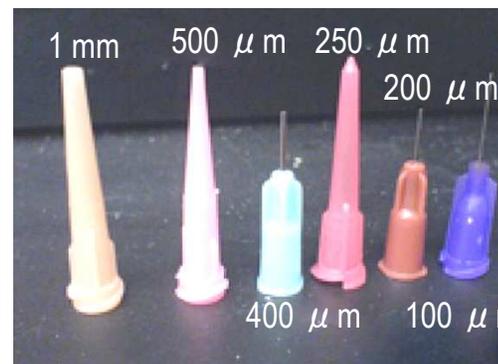
### Design Choice:

- Traditional technologies don't optimize for power output
- For waste heat sources, it is best to optimize for maximum power
  - Requires 100-500  $\mu\text{m}$  element sizes

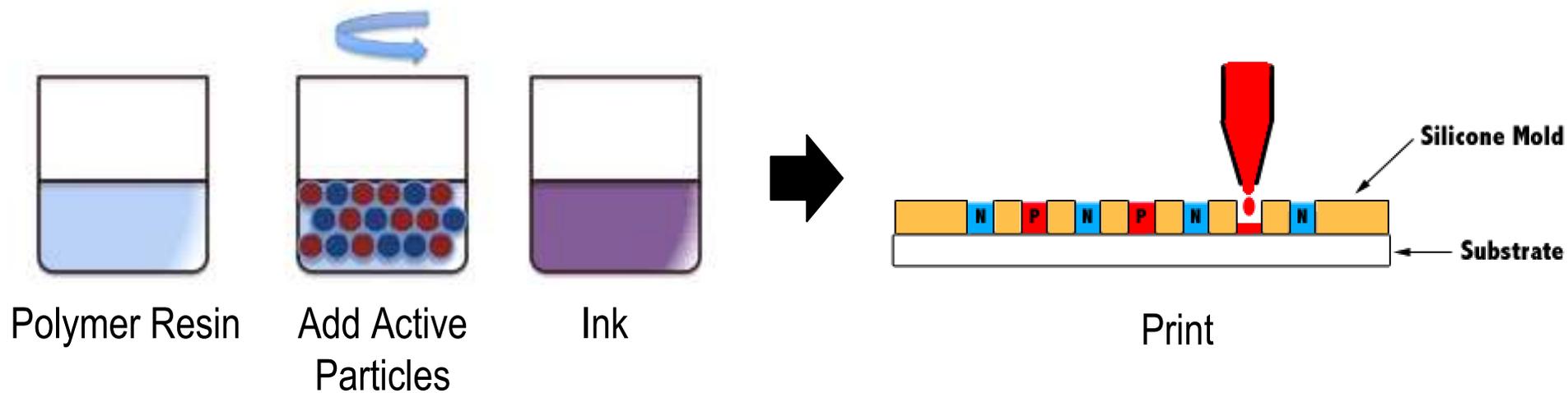
# Direct-Write Dispenser Printing



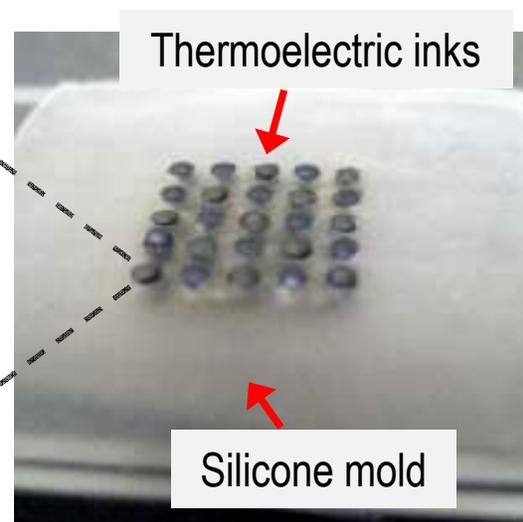
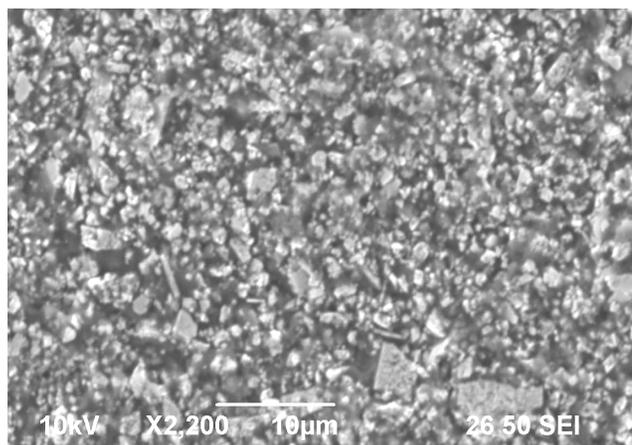
- 3 axis (X, Y, Z) Dispenser Printer
- 5  $\mu$  m resolution stage
- Feature size limited by syringe tip size



# Dispenser Printed Thermoelectrics



SEM Image of Printed Thermoelectric Materials



# Initial Material Properties

If bulk material properties could be retained ( $\Delta T = 10$  K):

Predicted Power =  $237.6 \mu\text{W}$ , Voltage =  $1.18$  V

**N-type  $\text{Bi}_2\text{Te}_3$**

$\alpha$  :  $195 \mu\text{V/K}$

$\rho$  :  $1.35\text{e-}5 \Omega\text{-m}$

$\lambda$  :  $1.4 \text{W/m-K}$

**P-type  $\text{Bi}_2\text{Te}_3$**

$\alpha$  :  $230 \mu\text{V/K}$

$\rho$  :  $1.75\text{e-}5 \Omega\text{-m}$

$\lambda$  :  $1.2 \text{W/m-K}$

**Bulk**

Current best material properties ( $\Delta T = 10$  K)

Predicted Power =  $61.2 \mu\text{W}$ , Voltage =  $1.33$  V

**N-type  $\text{Bi}_2\text{Te}_3$**

$\alpha$  :  $200 \mu\text{V/K}$

$\rho$  :  $2.5\text{e-}4 \Omega\text{-m}$

$\lambda$  :  $0.5 \text{W/m-K}$

**P-type  $\text{Bi}_{0.5}\text{Sb}_{1.5}\text{Te}_3$**

$\alpha$  :  $250 \mu\text{V/K}$

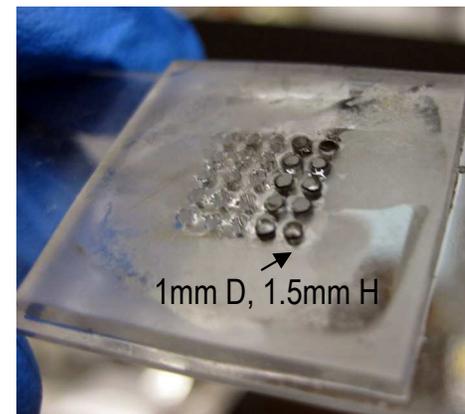
$\rho$  :  $2.5\text{e-}4 \Omega\text{-m}$

$\lambda$  :  $0.5 \text{W/m-K}$

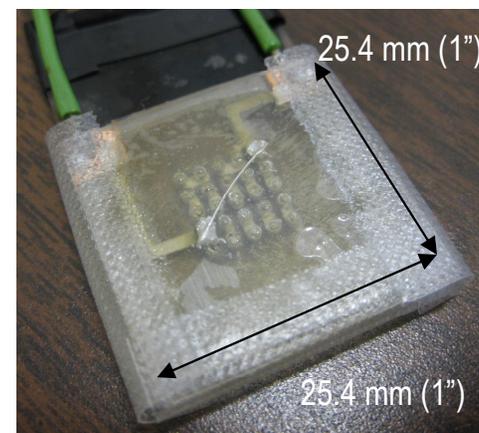
**Current**

# Preliminary Findings

- Existing bulk devices cannot meet the requirements for low waste heat sources to power
- Dispenser printing is a viable technique for creating the optimal size factors
- Initial materials show promising behavior
- Further work is being performed on materials optimization & device fabrication



Printed Thermoelectric Pillars

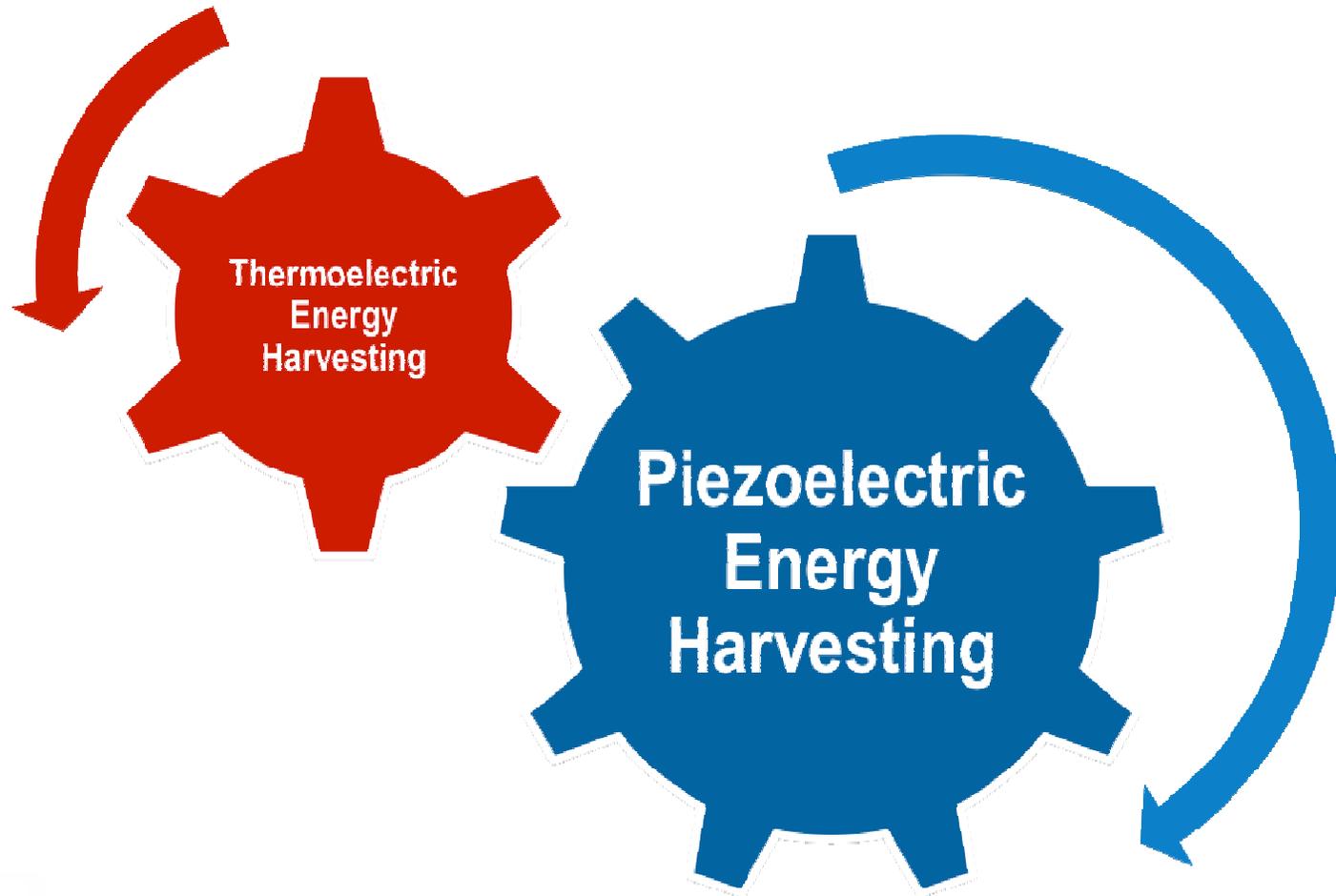


Device Prototype

Predicted Performance (10K gradient)

Picocube Demand	Predicted
Power : 10 $\mu$ W avg.	Power : 61 $\mu$ W.
Voltage : <b>0.7 V (DC conv)</b>	Voltage : <b>1.33 V</b>

# \*Switch gears\*



# Ambient Vibrations in the Built Environment

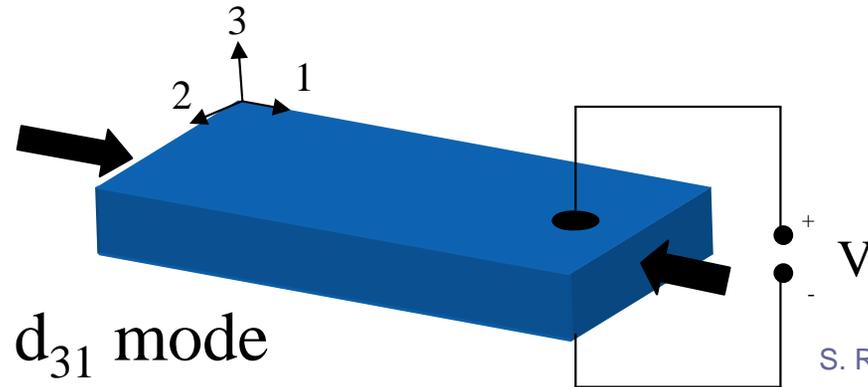
- Vibrations in buildings are low *acceleration*, low *frequency*

## Acceleration and frequency of several vibration sources in buildings

	acceleration (g's)	frequency (hz)
Washing machine	0.31	85
Clothes dryer	0.36	121
Small microwave oven	0.23	121
External windows by street	0.07	100
HVAC Etchevery roof	0.25	185
HVAC duct Etchevery 5th floor	0.34	29
Refrigerator	0.02	59

S. Roundy, PhD Thesis UC Berkeley 2003.  
Romy Fain, UC Berkeley undergraduate.

# Piezoelectricity



S. Roundy, PhD Thesis UC Berkeley 2003

$D_i$  = electric displacement

$S_i$  = strain

$T_i$  = stress

$E_i$  = electric field

$d_{31}$  = piezoelectric constant

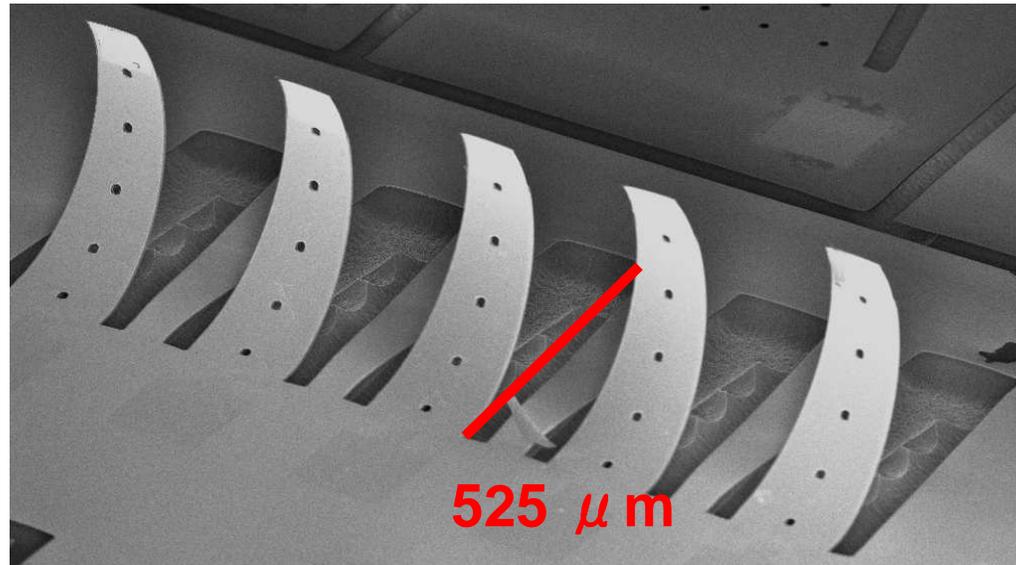
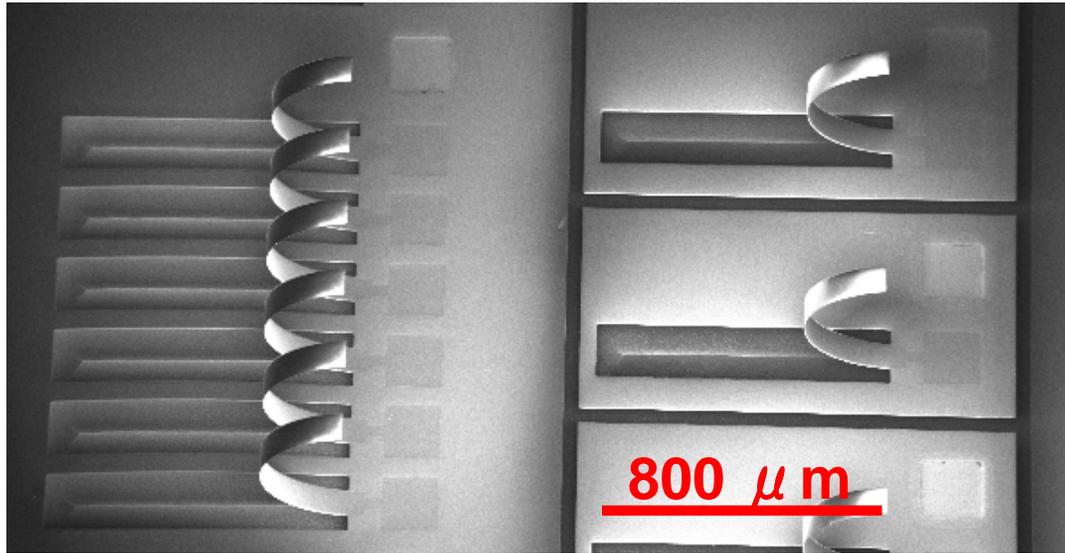
$\epsilon_{33}$  = permittivity (at constant stress)

$s_{11}$  = elastic compliance (at constant electric field)

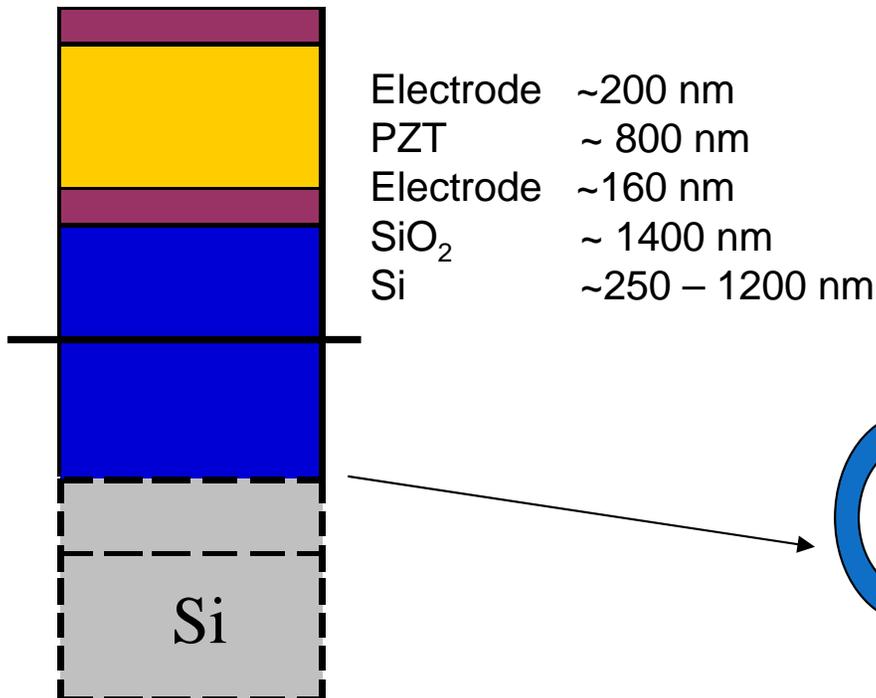
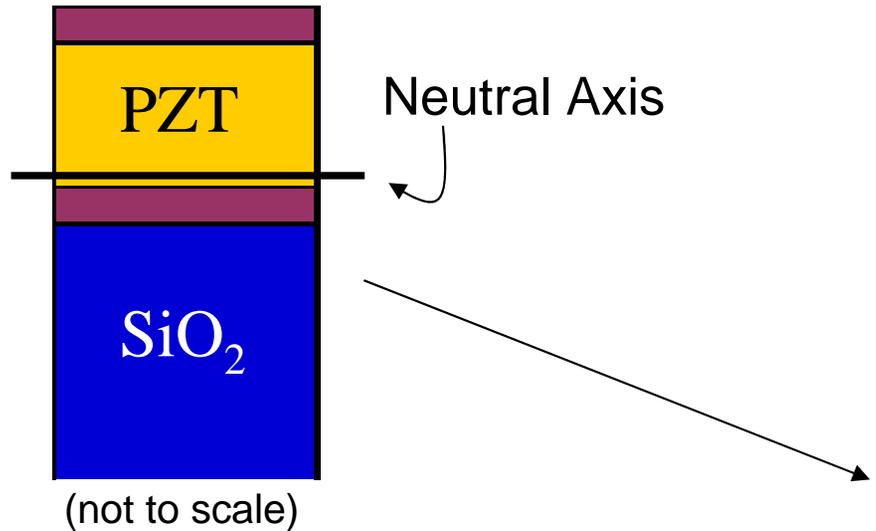
$$D_3 = d_{31}T_1 + \epsilon_{33}^T E_3$$

$$S_1 = s_{11}^E T_1 + d_{31} E_3$$

# First generation prototypes

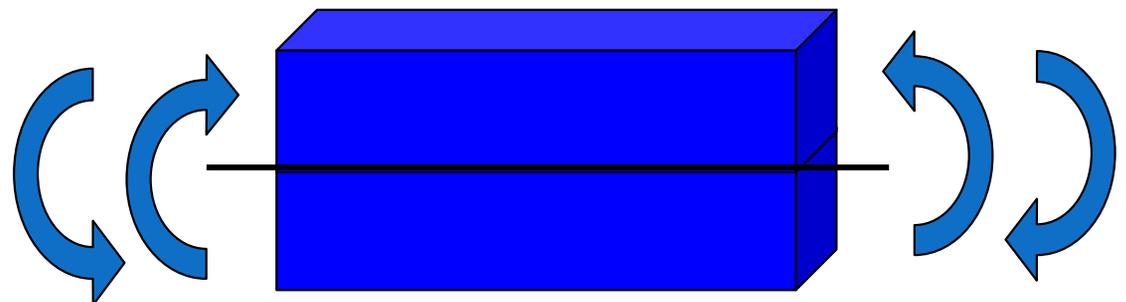
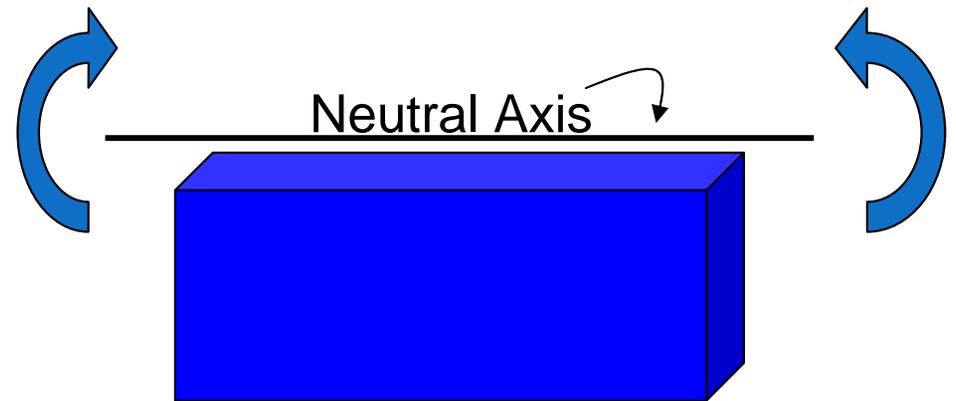


# Curvature of beams - stress compensation



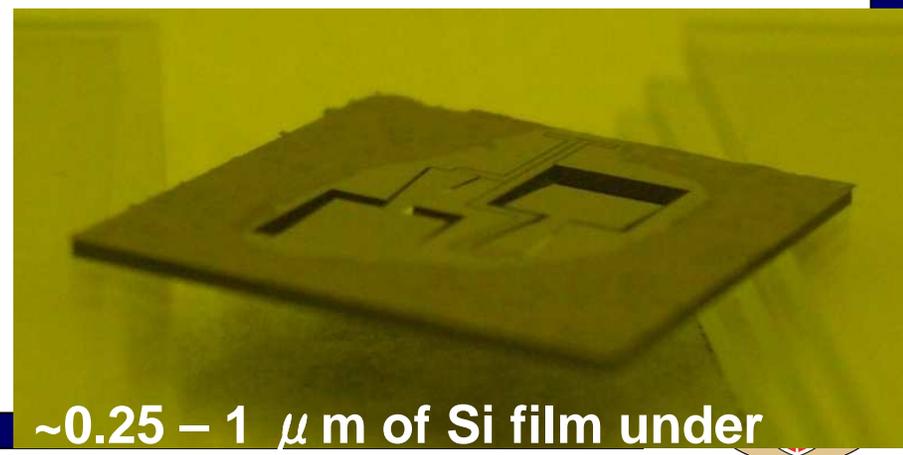
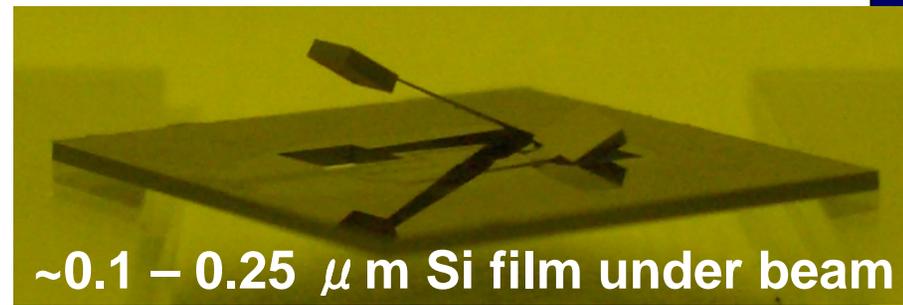
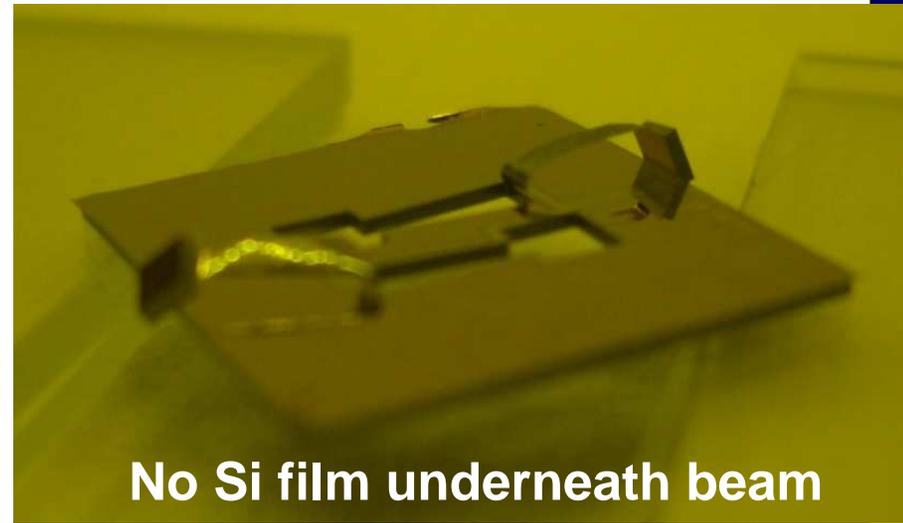
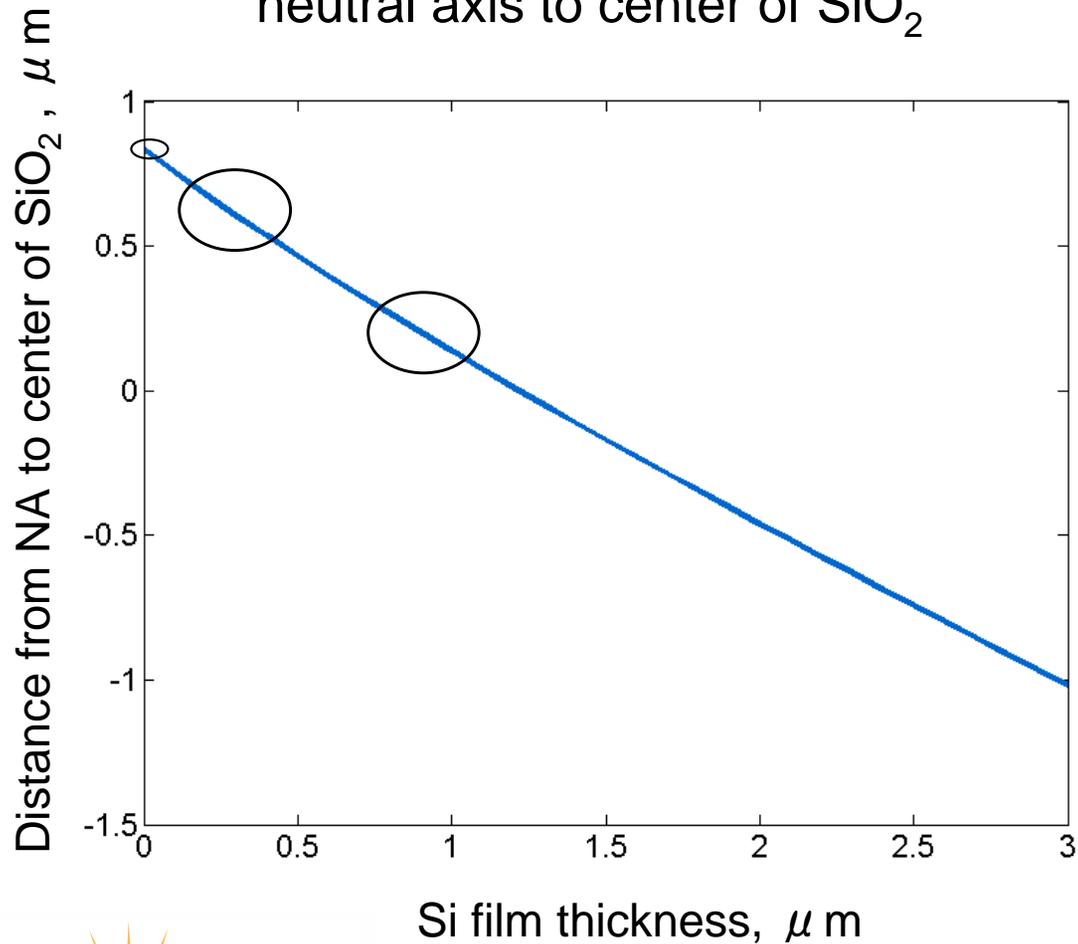
$$D_{ij} = \frac{1}{3} \sum_{k=1}^n (\overline{Q}_{ij})_k (z_k^3 - z_{k-1}^3)$$

$$\{M\} = [B]\{\epsilon^o\} + [D]\{\kappa\}$$



# Stress compensation results

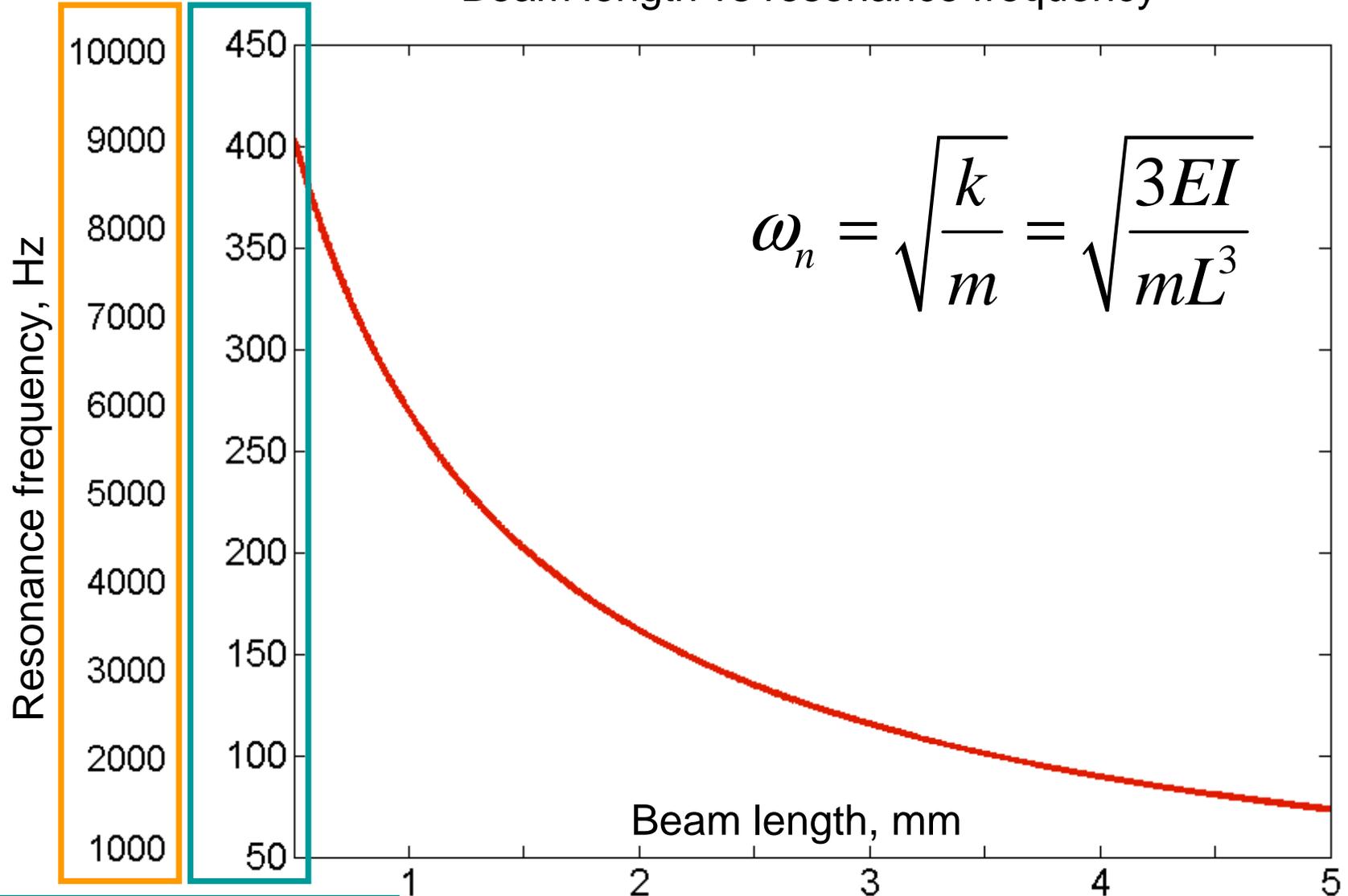
Si film thickness vs distance from neutral axis to center of SiO<sub>2</sub>



# Frequency reduction

3.2 e -15 m<sup>3</sup> Au mass

Beam length vs resonance frequency



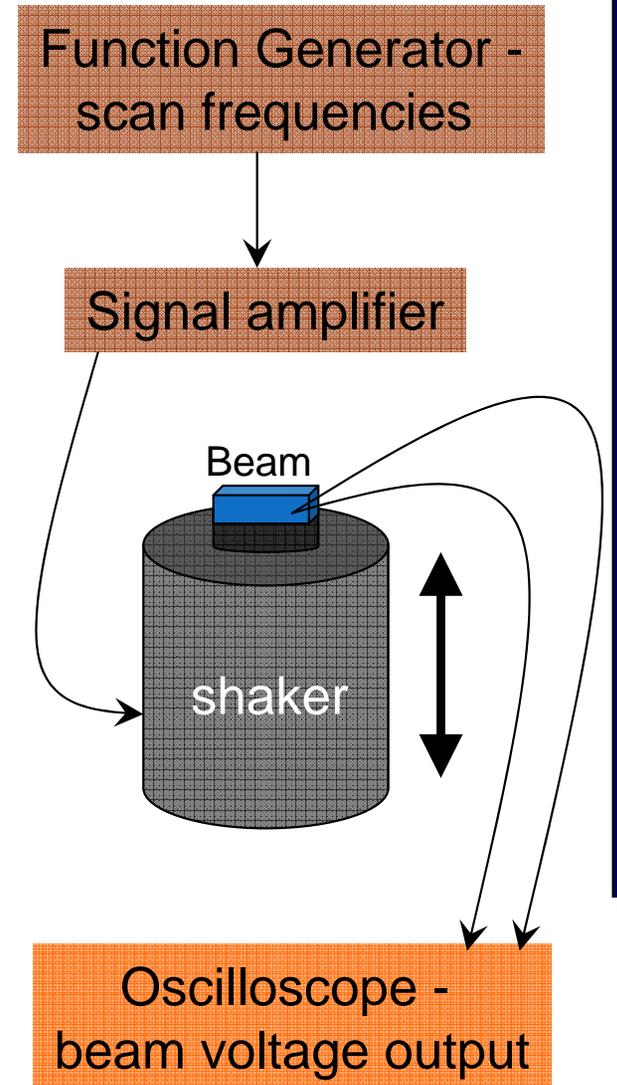
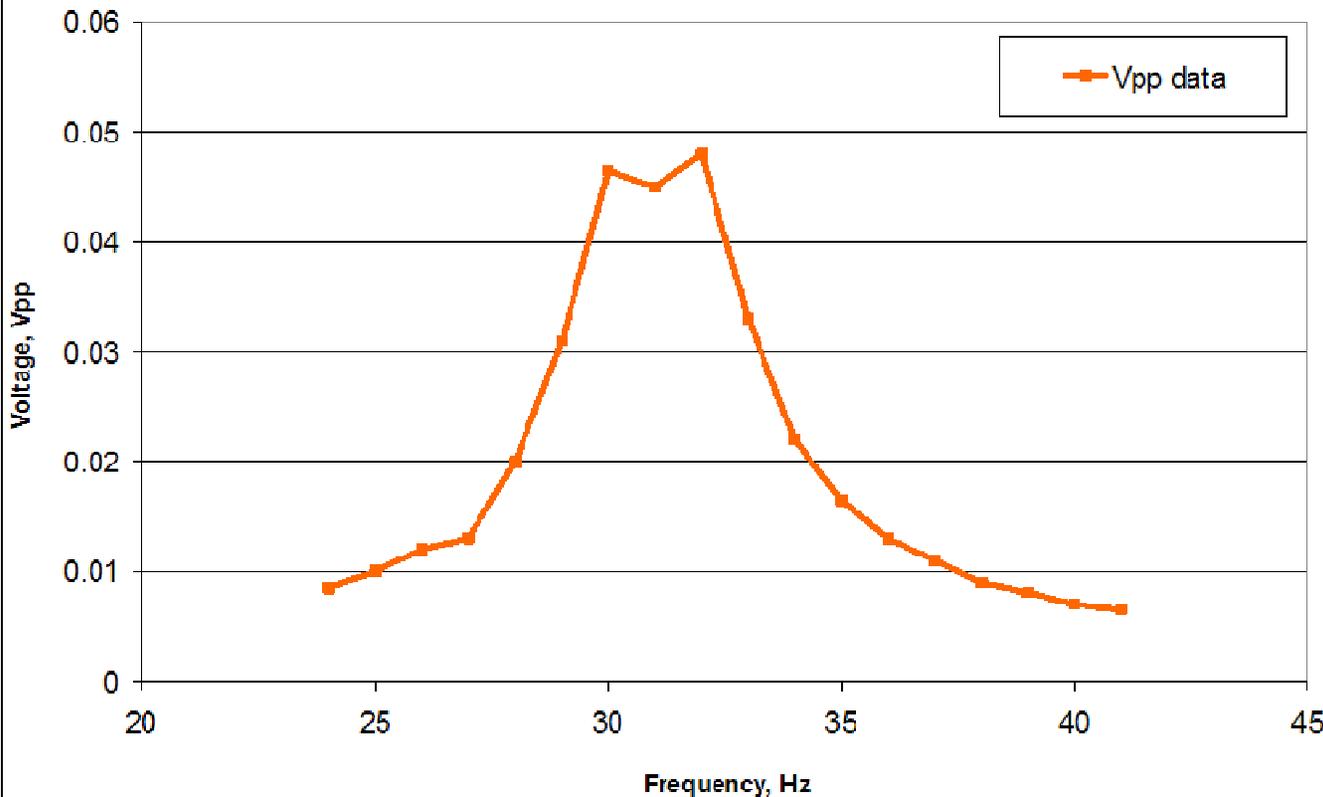
$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{3EI}{mL^3}}$$

5.25 e -10 m<sup>3</sup> Si mass

# Data confirms low resonance frequency

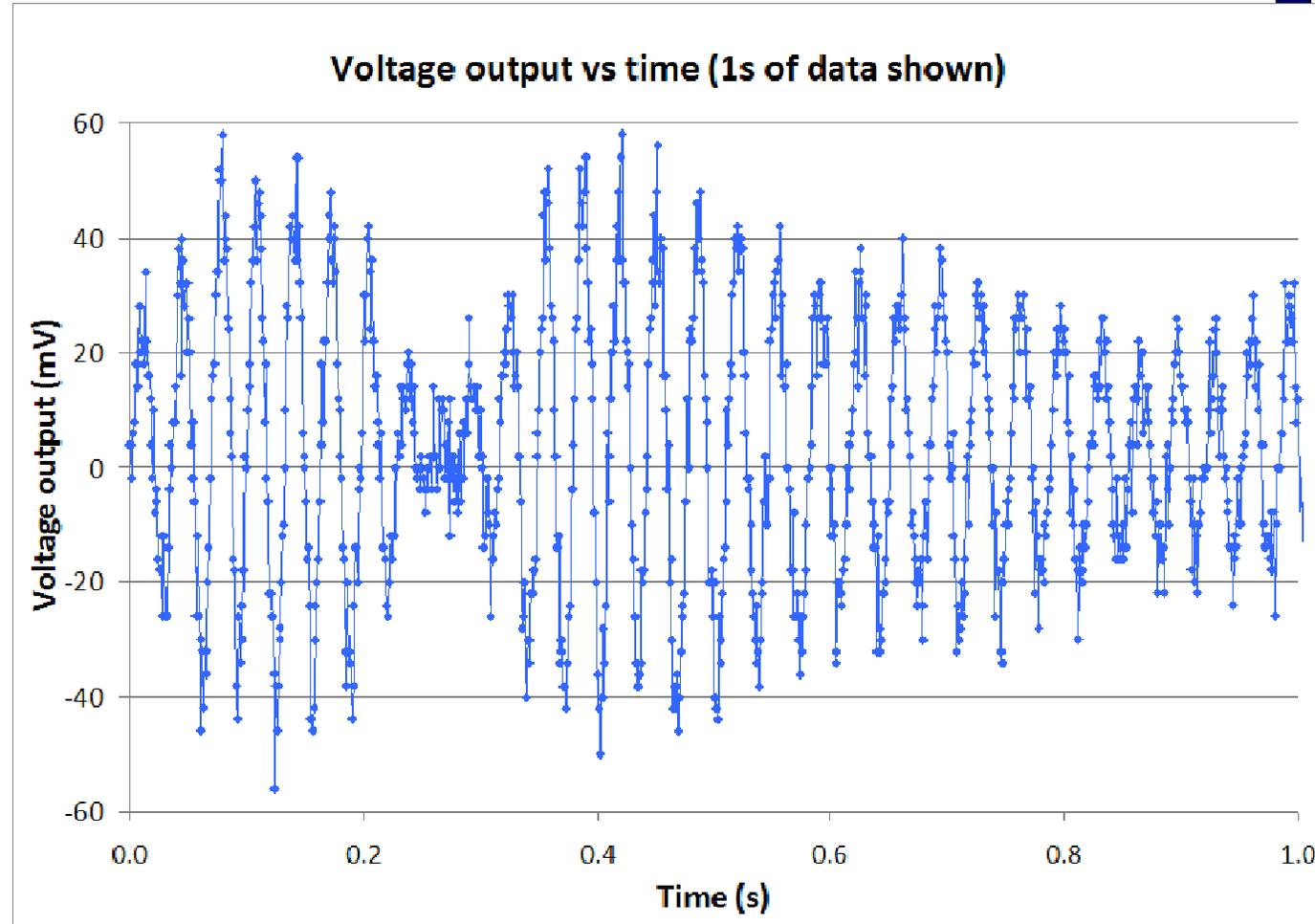
Model predicts 31 Hz if Si film  $t = 0.25$  microns, higher freq if Si film is thicker.

Voltage Output vs Frequency at  $3 \text{ m/s}^2$



# Preliminary results: ambient vibrations

Voltage output from energy harvester on duct  $\sim 22 \text{ mV}_{\text{rms}}$

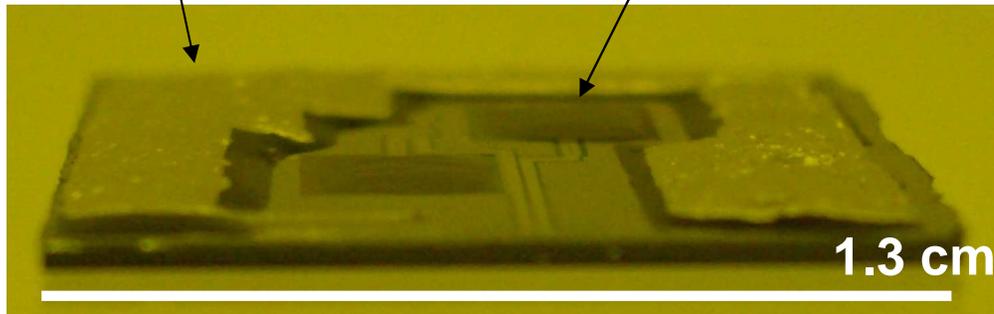


# Printed mass, printed capacitor

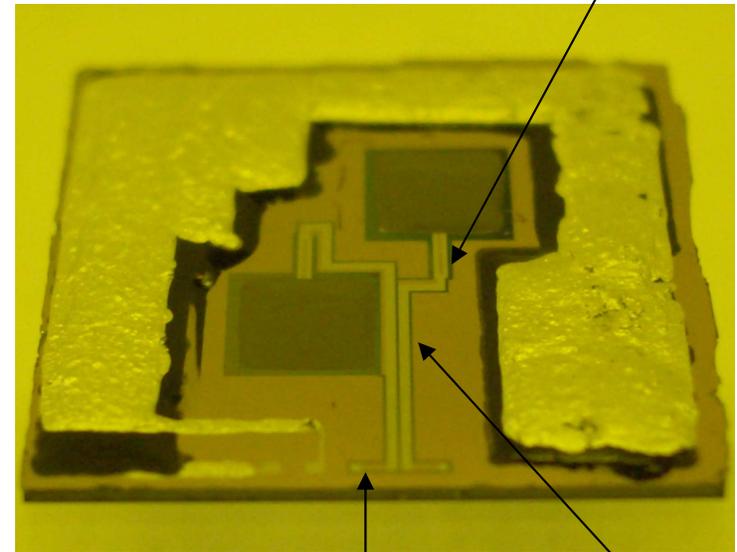
This is the first phase of work to integrate energy harvester with energy storage

Dispenser-printed capacitor sandwiched between current-collectors

Dispenser-printed proof mass



Beam structure



Electrode bond pads

Electrode leads

# Take-aways

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  - Composite materials show promise, further improvements under way
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# Thank you! Questions?

